



The fundamental diagram between  $u$  and  $k$  shows that as the density increase the speed will decrease. The flow will be 0 (zero) when the density is very high that it is not possible for the vehicle to move anymore. This situation is identified as jam density ( $k=k_j$ ). On the other hand, when the density is 0, the flow is also 0 because there is no vehicle in the road ( $q=0$ ). The characteristic between these two extreme points is the most essential that need to be known for traffic flow analysis.

As the density increases (from 0) the speed will decrease while the flow will increase. This will keep happen until it reaches a condition where the flow reach maximum and the increase of density will result on flow decrease. Such condition is known as flow capacity. Figure 1 also shows some essential parameter, defined as follows :  $q_m$  is capacity or maximum flow (vph),  $u_m$  is speed on flow capacity (mph),  $k_m$  is density on flow capacity (vpm),  $k_j$  is jam density (vpm) and  $u_{ff}$  is free flow speed (mph).

Data that can be observed from the field, by conducting traffic survey or by detector, are traffic flow and speed. In this study, there are 3 kinds of traffic flow model that were used to represent the mathematical relationship between the traffic flow, speed and density, which are, Greenshields model, Greenberg model and Underwood model

**Greenshields Model**

Greenshield formulated the mathematical relationship between speed and density as linear function [3], shown in equation 2 :

$$u = u_{ff} - \frac{u_{ff}}{k_j} k \tag{2}$$

Using equation (1), the relationship between flow and density was formulated and then by substituting (3) to (2), one can get the equation (4) and (5)

$$u = \frac{q}{k} \tag{3}$$

$$\frac{q}{k} = u_{ff} - \frac{u_{ff}}{k_j} k \tag{4}$$

$$q = k \cdot u_{ff} - \frac{u_{ff}}{k_j} k^2 \tag{5}$$

The equation (5) express the relationship between flow and density. Maximum Flow ( $q_m$ ) will be reached at the condition  $k=k_m$ , that is stated by (6) to (7).

$$\frac{\partial q}{\partial k} = u_{ff} - \frac{2 \cdot u_{ff}}{k_j} k_m = 0 \tag{6}$$

$$k_m = \frac{k_j}{2} \tag{7}$$

By substituting (7) to (5), the maximum flow ( $q_m$ ) is shown in equation (8),

$$q_m = \frac{k_j \cdot u_{ff}}{4} \tag{8}$$

The relationship between flow and speed can be formulated using equation (1) and by substituting (9) to (2), one can written equation (10) – (12)

$$k = \frac{q}{u} \tag{9}$$

$$u = u_{ff} - \frac{u_{ff}}{k_j} \cdot \frac{q}{u} \tag{10}$$

$$\frac{u_{ff}}{k_j} \cdot \frac{q}{u} = u_{ff} - u \tag{11}$$

$$q = k_j \cdot u - \frac{k_j}{u_{ff}} u^2 \tag{12}$$

Equation 12 stated the relationship between flow and speed. The maximum flow ( $q_m$ ) is reached when  $u=u_m$  as expressed in (13)-(14).

$$\frac{\partial q}{\partial u} = k_j - \frac{2 \cdot k_j}{u_{ff}} \cdot u_m = 0 \tag{13}$$

$$u_m = \frac{u_{ff}}{2} \tag{14}$$

By substituting (14) to (12), the  $q_m$  can be formulated as shown in (15) :

$$q_m = \frac{k_j \cdot u_{ff}}{4} \tag{15}$$

Thus, can be concluded that  $q_m$  can be reach when  $u=u_m$  and  $k=k_m$ .

**Greenberg Model**

Greenberg assumed the relationship between speed and density as logarithmic function (instead of linear function)[4] [3],

$$u = c \ln \left( \frac{k_j}{k} \right) \tag{16}$$

The equation (16) can be written as in (17), which is the speed and density relationship function :

$$u = c \ln k_j - c \ln k \tag{17}$$

The relationship between flow and speed can be formulated by substituting (17) to (1),

$$q = ck \ln k_j - ck \ln k \quad (18)$$

Equation (18) expresses the relationship between flow and density. Maximum flow ( $q_m$ ) can be reached when  $k=k_m$ .  $k=k_m$  is formulated in (22)-(24)

$$\frac{\partial q}{\partial k} = c \ln k_j - c(\ln k + 1) = 0 \quad (19)$$

$$\ln k_j = \ln k + 1 \quad (20)$$

$$\ln k = \ln k_j - 1 \quad (21)$$

$$k = k_j \cdot e^{-1} \quad (22)$$

The flow speed relationship can be formulated using equation (1), by substituting (9) to (17) one can formulated the equation (23) – (27)

$$u = c \ln k_j - c \ln \frac{q}{u} \quad (23)$$

$$c \ln \frac{q}{u} = c \ln k_j - u \quad (24)$$

$$\ln \frac{q}{u} = \ln k_j - \frac{u}{c} \quad (25)$$

$$\frac{q}{u} = k_j \cdot e^{-\frac{u}{c}} \quad (26)$$

$$q = u \cdot k_j \cdot e^{-\frac{u}{c}} \quad (27)$$

### Underwood Model

Underwood assumed the relationship between speed and density as exponential function. The basic formula for Underwood model can be stated by (28).

$$u = u_{ff} \cdot e^{-\frac{k}{k_m}} \quad (28)$$

Where  $u_{ff}$  = free flow speed and  $k_m$  = density on maximum flow condition (capacity). Equation (28) can be expressed in logarithmic natural form as shown in (29) which expresses the relationship between speed and density.

$$\ln u = \ln u_{ff} - \frac{k}{k_m} \quad (29)$$

The flow – density relationship can be formulated using the basic equation (1) and by substituting the equation (3) into (28) as shown in (30) – (31)

$$\frac{q}{k} = u_{ff} \cdot e^{-\frac{k}{k_m}} \quad (30)$$

$$q = k \cdot u_{ff} \cdot e^{-\frac{k}{k_m}} \quad (31)$$

Equation (31) expressed the relationship between flow and density. The maximum flow ( $q_m$ ) is reached as  $k=k_m$ . The flow speed relationship can be formulated using basic equation (1) and by substituting (9) into (28), as shown in (32) – (35).

$$u = u_{ff} \cdot e^{-\frac{q}{u \cdot k_m}} \quad (32)$$

$$\ln u = \ln u_{ff} - \frac{q}{u \cdot k_m} \quad (33)$$

$$\frac{q}{u \cdot k_m} = \ln u_{ff} - \ln u \quad (34)$$

$$q = u \cdot k_m \cdot (\ln u_{ff} - \ln u) \quad (35)$$

The equation (35) expressed the relationship between flow and speed. The maximum flow ( $q_m$ ) is reached as  $u=u_m$ .  $u=u_m$  is formulated in equation (36) – (39).

$$\frac{\partial q}{\partial u} = k_m(\ln u_{ff} - \ln u_m) + k_m \cdot u_m \left(-\frac{1}{u_m}\right) = 0 \quad (36)$$

$$k_m(\ln u_{ff} - \ln u_m) - k_m = 0 \quad (37)$$

$$(\ln u_{ff} - \ln u_m) = 1 \quad (38)$$

$$u_m = e^{\ln u_{ff} - 1} \quad (39)$$

### DATA

The data was taken from Virginia Department of Transportation website. The data is traffic flow data collected from road link I-64 Westbound at the upstream of Hampton Road Bridge Tunnel which is located before the bridge as shown by figure 2. This link has two lanes.



Figure 2. Road link I-64 Westbound

This study utilized twenty four hours traffic data (instead of just taken the AM peak and PM peak) to capture traffic flow characteristic in extreme situations both at free flow speed and traffic jam condition. The date of data collection is September 15, 2011. There are two parameters in the data which are traffic flow (vp15m) and speed (mph). In the data processing the traffic flow data was converted into vehicles per hour (vph) unit.

**Calibration of Greenshield, Greenberg and Underwood Model**

As has been discussed earlier, Greenshield equation for speed versus density form a linear function,

$$u = u_{ff} - \frac{u_{ff}}{k_j} k$$

Assume that  $u = Y$  and  $k = x$ , then the equation above can be written in linear equation  $Y = A + B.x$ , where  $A = u_{ff}$  and  $B = -\frac{u_{ff}}{k_j}$ . Unlike Greenshields, Greenberg equation for speed versus density form a logarithmic function,

$$u = c \ln\left(\frac{k_j}{k}\right) \Leftrightarrow u = c \ln k_j - c \ln k$$

Assume that  $u = Y$  and  $\ln k = x$ , then the equation above can be written in linear equation  $Y = A + B.x$ , where  $A = c \ln k_j$  and  $B = -c$ . In Underwood model, the speed versus density equation form an exponential function,

$$u = u_{ff} \cdot e^{-\frac{k}{k_m}} \Leftrightarrow \ln u = \ln u_{ff} - \frac{k}{k_m}$$

Assume that  $\ln u = Y$  and  $k = x$ , then the equation above can be written in linear equation  $Y = A + B.x$ , where  $A = \ln u_{ff}$  and  $B = -\frac{1}{k_m}$

**Traffic flow model**

The traffic flow models were formulated using Greenshields, Greenberg and Underwood model. The models were built using regression analyses that were conducted in SPSS. By utilizing the speed and density data, the Greenshields, Greenberg and Underwood model were attained through regression analysis according to the associated function. Table 1 presents result of the regression analysis.

There are at least three relationship obtain from the model, which are speed – density, flow – density and flow – speed relationship. Table 2 presents those relationships.

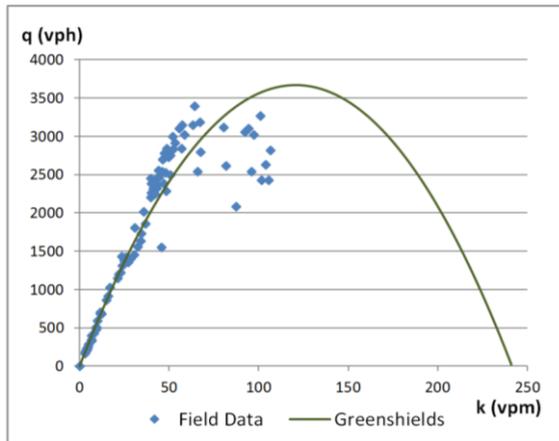
**Table 1. Regression Analysis Result**

	R <sup>2</sup>	A	B
Linear	0.559	60.822	-0.252
Logarithmic	0.232	66.022	-4.590
Exponential	0.571	63.690	-0.006

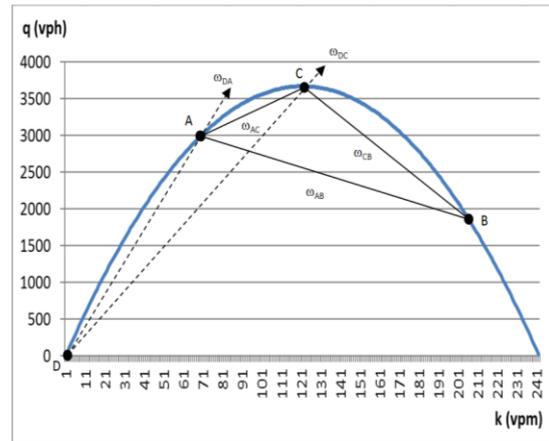
The chosen model was decided by looking at the coefficient determination (R<sup>2</sup>) of each model. As shown in table 1 the highest R<sup>2</sup> value is the exponential that represent Underwood model. However, beside the R<sup>2</sup> one would need to evaluate the characteristic offered by this model based on the fact in the field. This model would not work accurately when there is traffic jam condition, since the u-k curve never intersect with x-axis which is the density, thus the jam density (k<sub>j</sub>) would never be identified. Hence, by this consideration the chosen model in this case is Greenshields model. The plot of flow and density based on field data versus the one generated from Greenshields equation is presented by figure 3.a.

**Table 2. The relationship between traffic flow parameters**

	Speed - Density	Flow - Density	Flow - Speed
Greenshields	$u = 60.822 - 0.252 k$	$q = 60.822 k - 0.252 k^2$	$q = 241.357 u - 3.968 u^2$
Greenberg	$u = 66.022 - 4.59 \ln k$	$q = 66.022 k - 4.59 k \ln k$	$q = 1765383 u \cdot e^{-0.218 u}$
Underwood	$\ln u = 4.154 - 0.006 k$	$q = 63.69 k \cdot e^{-0.006 k}$	$q = 692.338 u - 166.667 u \ln u$



3.a. Field Data vs Greenshield q-k plot



3.b. Shockwave generated by lane closure

Figure 2. Greenshields q-k Diagram

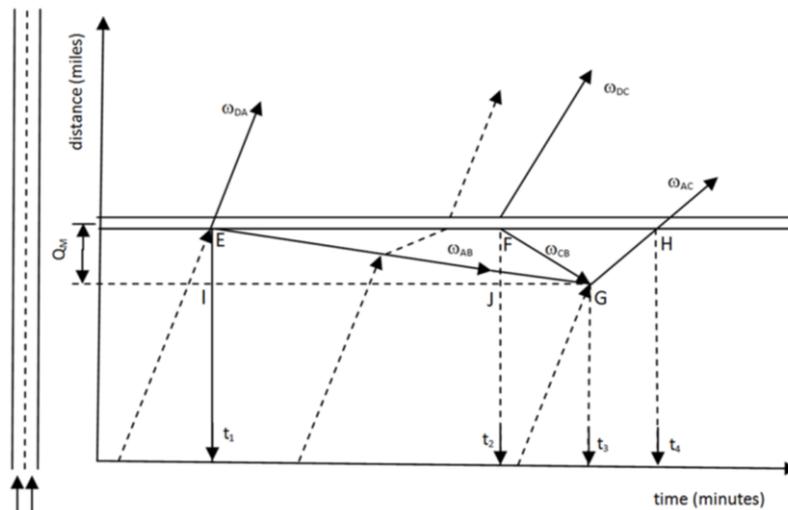


Figure 3. Time and space diagram

**Incident Scenario**

The shockwave in this study was analyzed using the following scenario; the incident happened when the traffic flow is constant at 3000 vph, 1 lane (out of 2) was closed due to incident. The link capacity is derived from Greenshield model which is 3670 vph, while the capacity of the link was generated from VISSIM simulation. The reason for doing that is, later the result from shockwave analysis will be compared to the VISSIM simulation result, thus to have a fair comparison the input should be identical.

**SHOCKWAVE ANALYSIS**

**Shockwave diagram**

Figure 3.b. shows the shockwave diagram as a result of lane closure. Point A showing the flow

and density at the moment the incident happened, due to the incident the flow decrease to one lane capacity (point B). Point C shows the flow and density at link capacity (3670 vph).

**Shockwave speed and time – space diagram**

There are 3 shockwaves in this case (see figure 3). The shockwaves speed are calculated as follows

$$\omega_{AB} = \frac{q_B - q_A}{k_B - k_A}$$

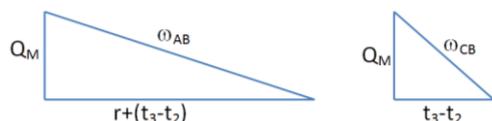
$$\omega_{CB} = \frac{q_B - q_C}{k_B - k_C}$$

$$\omega_{AC} = \frac{q_C - q_A}{k_C - k_A}$$

Using the shockwave diagram, the time - space diagram can be built as shown in figure 4.

$t_2-t_1$  shows the duration of incident,  $t_3-t_2$  is associated with the total time from lane opening to the time of last vehicle joining the queue,  $t_4-t_2$  is the total time from lane opening to normal condition and  $Q_M$  is the queue length. The total delay is the multiplication of EFG triangle area with density value associated with it and the multiplication FHG triangle area with density value related to it.

**Total time from lane opening to the time of last vehicle entering the queue**



If  $r$  = effective duration of lane closure ( $t_2-t_1$ ), than the  $t_3-t_2$  can be calculated as follow (see  $\Delta EGI$  and  $\Delta FGJ$ ),

$$\omega_{CB} = \frac{Q_M}{t_3-t_2} \quad ; \omega_{AB} = \frac{Q_M}{r+(t_3-t_2)}$$

$$Q_M = \omega_{CB}(t_3-t_2); Q_M = \omega_{AB}(r + (t_3-t_2))$$

$$Q_M = Q_M$$

$$\omega_{CB}(t_3-t_2) = \omega_{AB}(r + (t_3-t_2))$$

$$\omega_{CB}(t_3-t_2) = \omega_{AB} \cdot r + \omega_{AB}(t_3-t_2)$$

$$\omega_{CB} = \frac{\omega_{AB}(r)}{(t_3-t_2)} + \omega_{AB}$$

$$\omega_{CB} - \omega_{AB} = \frac{\omega_{AB} \cdot r}{t_3-t_2}$$

$$t_3-t_2 = \frac{\omega_{AB} \cdot r}{\omega_{CB} - \omega_{AB}}$$

$$t_3 - t_2 = \frac{r}{60} \frac{|\omega_{AB}|}{|\omega_{CB}| - |\omega_{AB}|} * 60$$

**Length of the queue (Q<sub>M</sub>)**

The queue length is calculated as follows,

$$Q_M = \omega_{CB} \cdot t_3 - t_2$$

$$Q_M = \frac{r}{60} \frac{|\omega_{CB}| \cdot |\omega_{AB}|}{|\omega_{CB}| - |\omega_{AB}|}$$

**Total time from lane opening to normal condition**

Using  $t_3-t_2$  and  $Q_M$  the total time from lane opening to normal condition is formulated as follow,

$$t_4 - t_3 = \frac{Q_M}{\omega_{AC}}$$

$$t_4 - t_2 = (t_4 - t_3) + (t_3 - t_2)$$

$$t_4 - t_2 = \frac{Q_M}{\omega_{AC}} + (t_3 - t_2)$$

**Total Delay**

Total Delay is the total area of EGH triangle with density, in this case total delay is multiplication of the area of triangle EFG and its density plus multiplication of the area of triangle FHG and its density

$$TD = \frac{r \cdot Q_M}{2} (k_B - k_A) + \frac{(t_4-t_2) \cdot Q_M}{2} + (k_C - k_A)$$

**Shockwaves in various scenarios**

Assumed that the arrival rate is 3000 vph, using the same procedure the shockwaves for 10 minutes lane closure are presented in table 3.

**Table 3 Shockwave for 1 lane closure**

Close d Lane	q <sub>A</sub> vph	k <sub>A</sub> vp m	u <sub>A</sub> mph	q <sub>E</sub> vph	k <sub>S</sub> vpm	u <sub>S</sub> mp h	w <sub>AS</sub> mph	q <sub>C</sub> vph	k <sub>C</sub> vpm	u <sub>C</sub> mph	w <sub>EC</sub> mph	w <sub>AC</sub> mph	r minut e	t <sub>3</sub> - t <sub>2</sub> minut e	Q <sub>M</sub> mile	t <sub>4</sub> - t <sub>2</sub> minut e	Total Delay veh.min	Total Delay veh.hr
1	3000	68.96	43.44	1823.00	206.58	8.76	-8.55	3670	115.45	31.73	20.27	14.41	10	7.30	2.47	7.47	2125.09	35.42
1	3000	68.96	43.44	1823.00	206.58	8.76	-8.55	3670	115.45	31.73	20.27	14.41	15	10.95	3.70	11.21	4781.46	79.69
1	3000	68.96	43.44	1823.00	206.58	8.76	-8.55	3670	115.45	31.73	20.27	14.41	20	14.60	4.93	14.94	8500.37	141.67
1	3000	68.96	43.44	1823.00	206.58	8.76	-8.55	3670	115.45	31.73	20.27	14.41	25	18.25	6.16	18.68	13281.83	221.36
1	3000	68.96	43.44	1823.00	206.58	8.76	-8.55	3670	115.45	31.73	20.27	14.41	30	21.90	7.40	22.41	19125.83	318.76
1	3000	68.96	43.44	1823.00	206.58	8.76	-8.55	3670	115.45	31.73	20.27	14.41	35	25.55	8.63	26.15	26032.38	433.87
1	3000	68.96	43.44	1823.00	206.58	8.76	-8.55	3670	115.45	31.73	20.27	14.41	40	29.20	9.86	29.88	34001.47	566.69
1	3000	68.96	43.44	1823.00	206.58	8.76	-8.55	3670	115.45	31.73	20.27	14.41	45	32.85	11.10	33.62	43033.12	717.22
1	3000	68.96	43.44	1823.00	206.58	8.76	-8.55	3670	115.45	31.73	20.27	14.41	50	36.50	12.33	37.35	53127.30	885.46
1	3000	68.96	43.44	1823.00	206.58	8.76	-8.55	3671	115.84	31.63	20.37	14.31	55	39.82	13.52	40.76	64064.67	1067.74
1	3000	68.96	43.44	1823.00	206.58	8.76	-8.55	3672	116.25	31.53	20.47	14.21	60	43.06	14.69	44.09	75964.04	1266.07

**Result Interpretation of Macroscopic Shockwaves Analysis**

By taking the  $\Delta$  (delta) of  $t_3 - t_2$ ,  $Q_M$  and  $t_4 - t_2$ , it can be concluded that every 5 minutes addition of incident duration will increase,

- the total time from lane opening to the time of last vehicle entering the queue for 3.65 minutes,
- the queue length for 1.23 miles, and
- the total time from lane opening to normal condition for 3.74 minutes

While the total delay increase exponentially (in the power of 3) as it is resulted of the multiplication of area and density.

**Modeling using VISSIM**

After get the result from macroscopic shockwave analysis, a shockwave simulation using transportation software “VISSIM” was built. The aim of this simulation is two compare the result of macroscopic shockwave analysis, particularly the queue length, with the shockwave resulted from microscopic traffic simulation. The data input for this simulation is network and demand. The network is a single link with two lanes, the link length is 99562.455 ft (18.86 miles), while the demand is 3000 vph and the simulation period is 3 hours.

The incident was created at downstream by installing a traffic signal in one of the lanes. The type of the signal control is fixed time and signal sequence is just red and green. The incident introduced when the traffic light turn to red from green which is setup to give enough time for the vehicles to reach the incident location. At the same place with traffic light, another VISSIM tools was fixed which is queue counters. The queue counters count the queue length (in ft) upstream from the location of traffic signal.

**Calibration**

It is unlikely that the result of VISSIM simulation will be the same with the of macroscopic shockwave analysis at first attempt, thus some calibrations need to take place. First thing that need to be calibrated is the capacity of a single lane next to the closed lane. By fixing data collection at associated point, the capacity of a link can be attained. The capacity of the single lane is 1823 vph which is the average of 20 times multirun. This number replaced the prior single lane capacity ( $q_B$ ) in macroscopic shockwave

analysis (which in the beginning was assumed to be a half of two lanes capacity).

Next step is calibrating the parameter for queue measurement VISSIM which is the queue definition. The queue definition for this simulation follows the following rule; vehicle will be defined as queuing vehicle when its speed is less than 5.0 mph and this situation end when its speed is greater than 7.0 mph. Other parameter needed to be calibrated in VISSIM is vehicle composition. There are three component of this parameter that affected the result significantly which are vehicle type, composition and desired speed. The vehicle types for this simulation are car, HGV (truck) and bus, which was assigned based on the situation in the field. The desired speed was assigned based on the speed of macroscopic shockwave analysis (43.44 mph at the flow = 3000 vph) which is 42.3 to 48.5 mph for car, 36.0 to 42.3 mph for both HGV and bus, while the relative flow (percentage of each type of vehicle) were assigned using trial and error method to find the optimal composition. The compositions of vehicle in this simulation are distributed as follows, 87% vehicles are car, 15% vehicles are HGV (truck) and 3% vehicles are bus.

**Comparison Result**

In order to have representative data, each incident duration was simulated for 10 times using the multirun simulation feature in VISSIM. As mentioned before the expected output is queue length. The result is summarized in table 4.

**Table 4 The Queue Length Comparison**

Incident Duration	$Q_M$ (VISSIM)		$Q_M$ Macroscopic	%dif ( $Q_M$ vs Average)
	max	average		
10	2.78	2.16	2.47	0.12
15	4.59	3.41	3.70	0.08
20	5.87	4.32	4.93	0.12
25	7.19	5.57	6.16	0.10
30	8.20	6.54	7.40	0.12
35	9.40	7.69	8.63	0.11
40	10.61	8.98	9.86	0.09
45	12.42	10.18	11.10	0.08
50	12.98	11.13	12.33	0.10
55	14.32	12.24	13.52	0.09
60	15.49	13.37	14.69	0.09

Table 4 also shows the comparison of queue length resulted from macroscopic shockwave analysis and the one resulted from traffic simulation in VISSIM. The maximum percentage difference between  $Q_M$  average from 10 simulation runs and  $Q_M$  Macroscopic is 12% while the minimum is 8% which shows a good match between the two analyses.

### CONCLUSION

Using the field data, the Greenshields, Greenberg and Underwood model have been calibrated in this study. In this particular location of study the Underwood model is the best model that fit the data however this model cannot deal with the traffic jam situation, thus for shockwaves analysis the Greenshields model is considered as the best

that represent the field data. The shockwave analysis was built using the Greenshields fundamental diagram have shown that the queue length, the total time from lane opening to the time of last vehicle entering the queue and the total time from lane opening to normal condition will increase linearly as the incident duration increase, while the total delay will increase exponentially. Through microscopic simulation established in VISSIM, the queue length also increase as the incident duration increase however the increase is not linear. In this study, the microscopic model has been calibrated successfully to meet the result of macroscopic shockwave analysis, particularly the queue length, and the important calibration factors in this study are speed distribution and vehicle composition.

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